

Lecture # 06: Conservation of Mass

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❑ **Feed back of the In-class Quiz #1 (43 response)**

- **Class teaching speed:**

- *Speed is okay: ~50%*
- *Speed is too fast: ~45%*
- *Speed is too slow: ~ 5%*

- **Other comments:**

- *Fast-paced with many derivations.*
- *Some mathematical terms can be expanded upon and explained more thoroughly*
- *Why use complicated formula to describe simple problems.*
- *More examples to link the equations to real word applications.*
- *More Practice problems on the slides, which can help prepare for HW and Tests.*

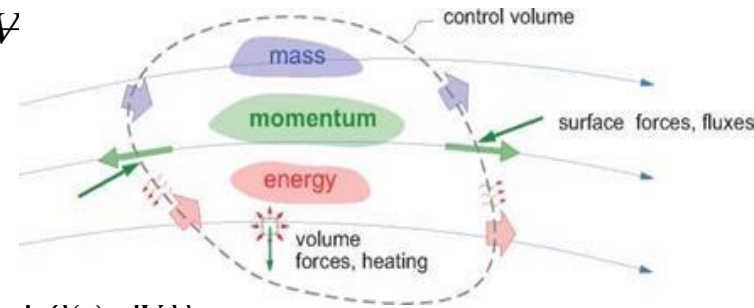
Reynolds Transport Theorem

- Let N be any extensive property of the identifiable fixed mass (system) such as total mass, momentum, or energy. The corresponding intensive property (extensive property per unit mass) will be designated as, α :

$$N \Big|_{\text{system}} = \int_{\text{system}} \alpha dm = \int_{\mathcal{V}} \alpha \rho d\mathcal{V}$$

- The rate of change of N can be written:

$$\frac{DN}{Dt} \Big|_{\text{system}} = \lim_{\delta t \rightarrow 0} \left\{ \frac{1}{\delta t} \left[\int_{\mathcal{V}(t+\delta t)} \alpha(t+\delta t) \rho(t+\delta t) d\mathcal{V} - \int_{\mathcal{V}(t)} \alpha(t) \rho(t) d\mathcal{V} \right] \right\}$$



If we make: $\beta(t) = \alpha(t)\rho(t)$

$$\frac{DN}{Dt} \Big|_{\text{system}} = \lim_{\delta t \rightarrow 0} \left\{ \frac{1}{\delta t} \left[\int_{\mathcal{V}(t+\delta t)} \beta(t+\delta t) d\mathcal{V} - \int_{\mathcal{V}(t)} \beta(t) d\mathcal{V} \right] \right\}$$

$$\frac{DN}{Dt} \Big|_{\text{system}} = \frac{D \int_{\mathcal{V}} \beta d\mathcal{V}}{Dt} = \lim_{\delta t \rightarrow 0} \left\{ \frac{1}{\delta t} \left[\int_{\mathcal{V}(t+\delta t)} \beta(t+\delta t) d\mathcal{V} - \int_{\mathcal{V}(t)} \beta(t+\delta t) d\mathcal{V} + \int_{\mathcal{V}(t)} \beta(t+\delta t) d\mathcal{V} - \int_{\mathcal{V}(t)} \beta(t) d\mathcal{V} \right] \right\}$$

$$= \lim_{\delta t \rightarrow 0} \left\{ \frac{1}{\delta t} \left[\overbrace{\int_{\mathcal{V}(t+\delta t)} \beta(t+\delta t) d\mathcal{V} - \int_{\mathcal{V}(t)} \beta(t+\delta t) d\mathcal{V}}^{\text{first two}} + \overbrace{\int_{\mathcal{V}(t)} \beta(t+\delta t) d\mathcal{V} - \int_{\mathcal{V}(t)} \beta(t) d\mathcal{V}}^{\text{second two}} \right] \right\}$$

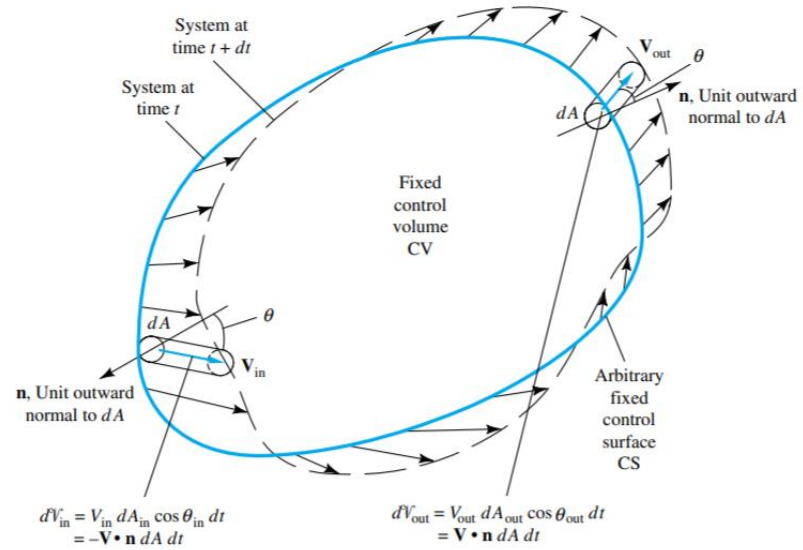
$$= \lim_{\delta t \rightarrow 0} \left\{ \frac{1}{\delta t} \left(\overbrace{\int_{\mathcal{V}(t+\delta t)} \beta(t+\delta t) d\mathcal{V} - \int_{\mathcal{V}(t)} \beta(t+\delta t) d\mathcal{V}}^{\text{first two}} \right) + \frac{\partial}{\partial t} \int_{\mathcal{V}} \beta d\mathcal{V} \right\}$$

$$= \lim_{\delta t \rightarrow 0} \left\{ \frac{1}{\delta t} \left(\int_{S(t)} \beta(t+\delta t) (\vec{V} \cdot \hat{e}_n) \delta t dA \right) + \frac{\partial}{\partial t} \int_{\mathcal{V}} \beta d\mathcal{V} \right\}$$

$$= \lim_{\delta t \rightarrow 0} \left(\int_{S(t)} \beta(t+\delta t) (\vec{V} \cdot \hat{e}_n) dA \right) + \frac{\partial}{\partial t} \int_{\mathcal{V}} \beta d\mathcal{V}$$

$$= \int_{C.S(t)} \beta(t) (\vec{V} \cdot \hat{e}_n) dA + \frac{\partial}{\partial t} \int_{\mathcal{V}} \beta d\mathcal{V}$$

$$= \int_{C.S} \beta \vec{V} \cdot d\vec{A} + \frac{\partial}{\partial t} \int_{\mathcal{V}} \beta d\mathcal{V} = \int_{C.S} \alpha \rho \vec{V} \cdot d\vec{A} + \frac{\partial}{\partial t} \int_{\mathcal{V}} \alpha \rho d\mathcal{V}$$

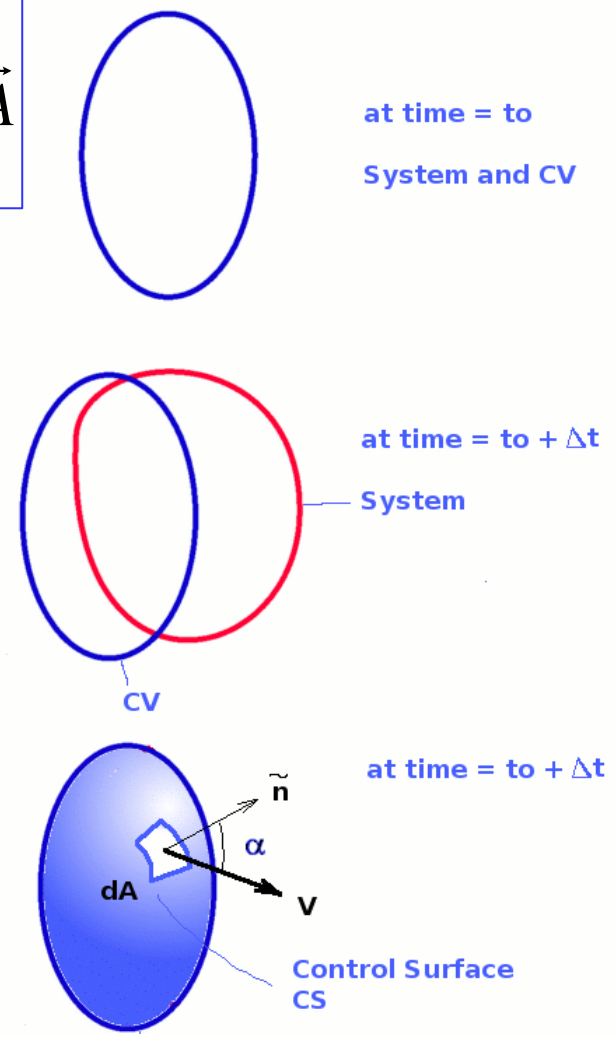
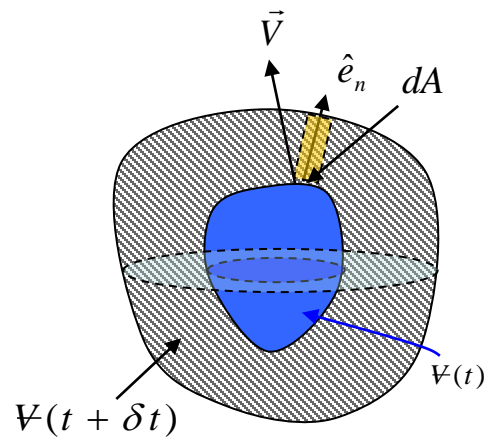


Reynolds Transport Theorem

$$\frac{DN_s}{Dt} = \frac{D \int_V \alpha \rho dV}{Dt} = \frac{\partial}{\partial t} \int_{C.V.} \alpha \rho dV + \int_{C.S.} (\alpha \rho \vec{V}) \cdot d\vec{A}$$

Where α is any intensive property corresponding to N . (i.e., $\alpha = N$ per unit mass), and it can be used for different quantities as follows.

N_s	α
Mass	1
Linear momentum	\vec{V}
Angular momentum	$\vec{R} \times \vec{V}$
Energy	e
Entropy	s

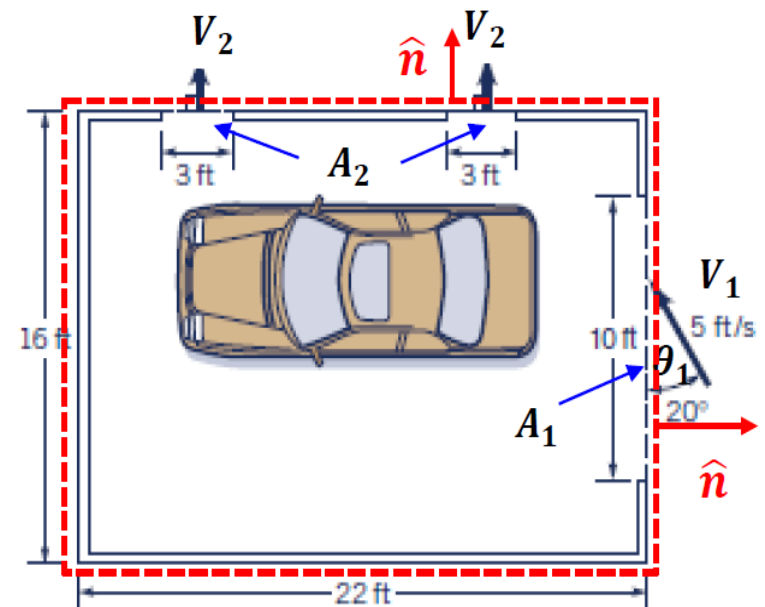


□ Integral Form of the Mass Conservation Equation

- Wind blows through a 7ft × 10ft garage door opening with speed of $V_1 = 5 \text{ ft/s}$ as shown in figure below. Determine the average speed, V_2 , of the air through the two 3 ft × 4ft window openings.

Solution procedure

- Choose and draw an appropriate control volume (the simplest CV along the surfaces we have information on or need to find)
- Write conservation law(s) for the chosen CV
- Evaluate volume integrals over the entire CV volume and surface integrals over control surfaces
- Simplify to find the unknown quantity



Fixed CV

Integral Form of the Mass Conservation Equation

Conservation of mass

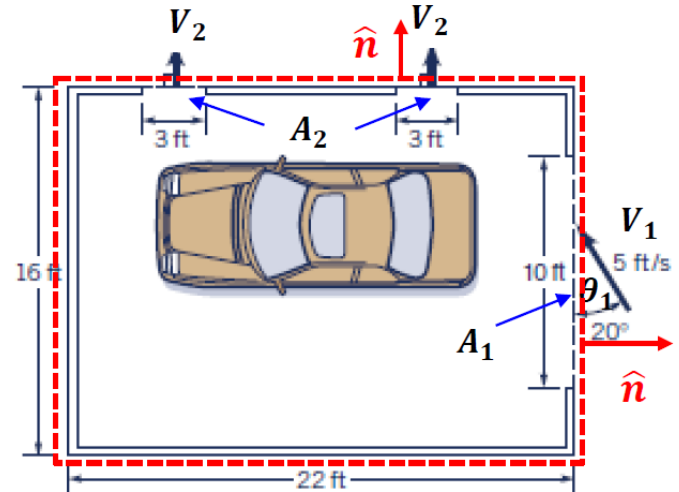
$$\frac{\partial}{\partial t} \iiint_V \rho dV + \iint_S \rho \vec{V} \cdot \hat{n} dS = 0$$

Here we can assume steady state condition (wind steadily blows in and leaves through the windows), hence

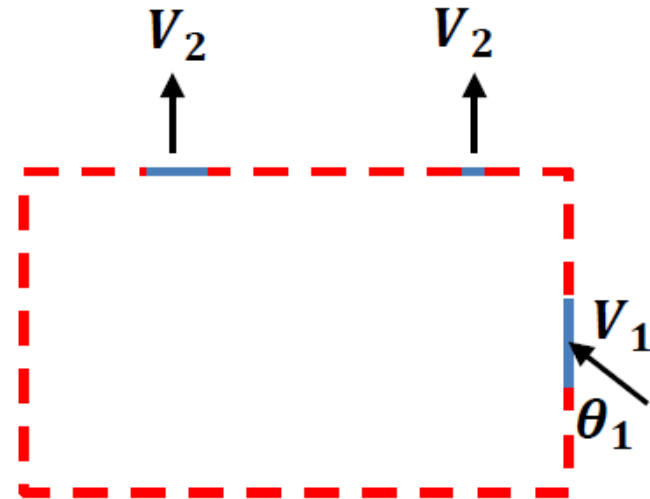
$$\frac{\partial}{\partial t} \iiint_V \rho dV = 0$$

$$\iint_S \rho \vec{V} \cdot \hat{n} dS = \iint_{A_1} \rho \vec{V} \cdot \hat{n} dS + 2 \iint_{A_2} \rho \vec{V} \cdot \hat{n} dS$$

Note: there are two identical windows, so it is reasonable to assume average velocity is the same through both.



Fixed CV



$$\iint_{A_1} \rho \vec{V} \cdot \hat{n} dS = \iint_{A_1} \rho V_1 (-\sin(\theta) \hat{i} + \cos(\theta) \hat{j}) \cdot \hat{i} dS$$

$$= -\rho V_1 \sin(\theta) \iint_{A_1} dS = -\rho V_1 \sin(\theta) A_1$$

$$\iint_{A_2} \rho \vec{V} \cdot \hat{n} dS = \iint_{A_2} \rho V_2 \hat{j} \cdot \hat{j} dS = \rho V_2 A_2$$

• $\sin(20) \approx 0.342$

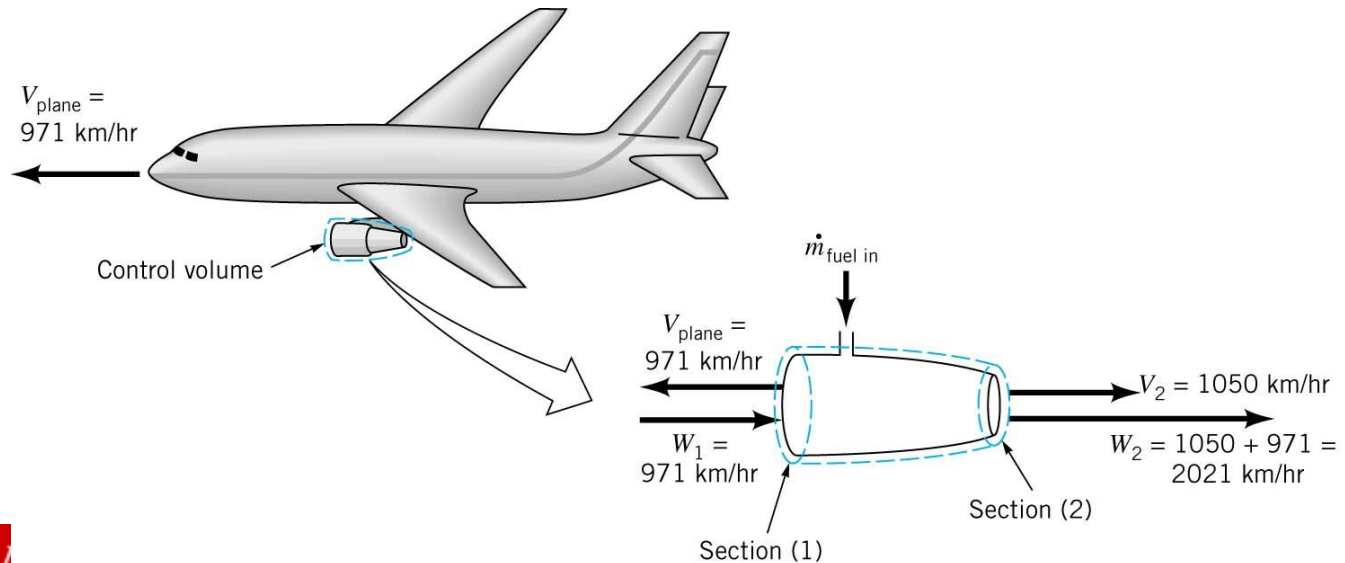
Therefore, conservation of mass becomes

$$-\rho V_1 \sin(\theta) A_1 + 2\rho V_2 A_2 = 0 \rightarrow V_2 = V_1 \sin(\theta) \frac{A_1}{2A_2}$$

$$V_2 = 5 \times \sin(20) \times \frac{10 \times 7}{2 \times 3 \times 4} \rightarrow V_2 = 4.99 \text{ ft/s}$$

□ Integral Form of the Mass Conservation Equation

- An airplane moves forward at a speed of 971 km/hr. The frontal area of the intake to one of the jet engines is 0.80m^2 , and the entering air density is 0.736 kg/m^3 . A stationary observer estimates that relative to earth, the jet engine exhaust gases move away from the engine with a speed of 1,050 km/hr. The engine exhaust area is 0.558 m^2 and the exhaust gas density is 0.515 kg/m^3 .
 - Question: Please estimate the mass flow rate of fuel into the engine in kg/hr.**



Integral Form of the Mass Conservation Equation

0 (flow relative to moving control volume is considered steady on a time-average basis)

$$\frac{\partial}{\partial t} \int_{cv} \rho dV + \int_{cs} \rho \mathbf{W} \cdot \hat{\mathbf{n}} dA = 0$$

Assuming one-dimensional flow, we evaluate the surface integral in Eq. 1 and get

$$-\dot{m}_{\text{fuel in}} - \rho_1 A_1 W_1 + \rho_2 A_2 W_2 = 0$$

or

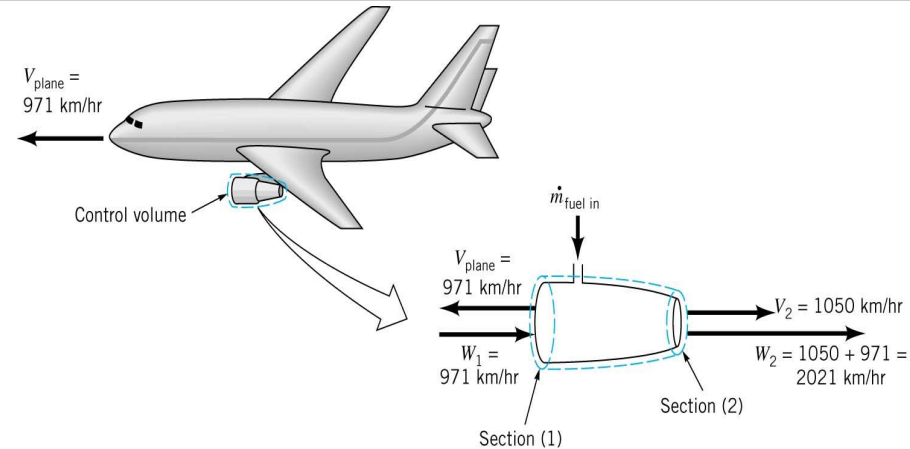
$$\dot{m}_{\text{fuel in}} = \rho_2 A_2 W_2 - \rho_1 A_1 W_1$$

We consider the intake velocity, W_1 , relative to the moving control volume, as being equal in magnitude to the speed of the airplane, 971 km/hr. The exhaust velocity, W_2 , also needs to be measured relative to the moving control volume. Since a fixed observer noted that the exhaust gases were moving away from the engine at a speed of 1050 km/hr, the speed of the exhaust gases relative to the moving control volume, W_2 , is determined as follows by using Eq. 5.14

$$V_2 = W_2 + V_{\text{plane}}$$

or

$$W_2 = V_2 - V_{\text{plane}} = 1050 \text{ km/hr} + 971 \text{ km/hr} = 2021 \text{ km/hr}$$



From Eq. 2,

$$\begin{aligned} \dot{m}_{\text{fuel in}} &= (0.515 \text{ kg/m}^3)(0.558 \text{ m}^2)(2021 \text{ km/hr})(1000 \text{ m/km}) \\ &\quad - (0.736 \text{ kg/m}^3)(0.80 \text{ m}^2)(971 \text{ km/hr})(1000 \text{ m/km}) \\ &= (580,800 - 571,700) \text{ kg/hr} \end{aligned}$$

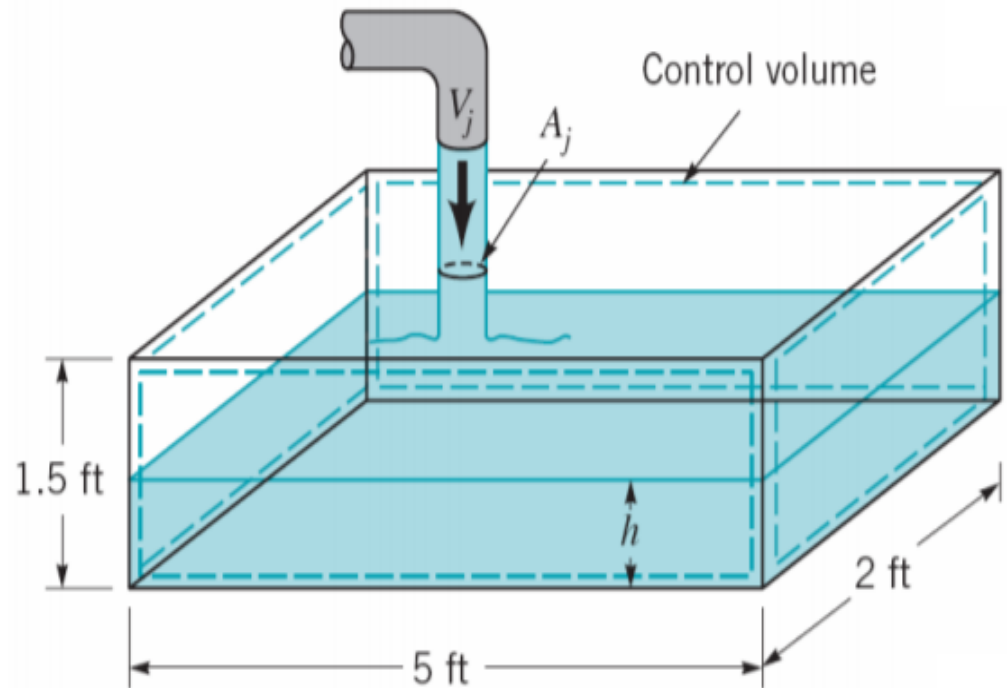
$$\dot{m}_{\text{fuel in}} = 9100 \text{ kg/hr}$$

(Ans)

Note that the fuel flowrate was obtained as the difference of two large, nearly equal numbers. Precise values of W_2 and W_1 are needed to obtain a modestly accurate value of $\dot{m}_{\text{fuel in}}$.

□ Integral Form of the Mas Conservation Equation

- A bathtub is being filled with water from a faucet. The rate of flow from the faucet is steady at 9 gal/min. The tub volume is approximated by a rectangular space as indicate the figure. Please estimate the time rate of change of the depth of water in at any instant.***



Integral Form of the Mass Conservation Equation

- Conservation of mass equation**

The continuity equation

$$\frac{\partial}{\partial t} \int_{CV} \rho dV + \int_{CS} \rho \vec{V} \cdot \vec{n} dA = 0$$

$$= \frac{\partial}{\partial t} \int_{\text{air volume}} \rho_{\text{air}} dV_{\text{air}} + \frac{\partial}{\partial t} \int_{\text{water volume}} \rho_{\text{water}} dV_{\text{water}} - \dot{m}_{\text{water}} + \dot{m}_{\text{air}}$$

For air $\frac{\partial}{\partial t} \int_{\text{air volume}} \rho_{\text{air}} dV_{\text{air}} + \dot{m}_{\text{air}} = 0$

For water $\frac{\partial}{\partial t} \int_{\text{water volume}} \rho_{\text{water}} dV_{\text{water}} = \dot{m}_{\text{water}}$

$$\int_{\text{water volume}} \rho_{\text{water}} dV_{\text{water}} = \rho_{\text{water}} [h(2\text{ft})(5\text{ft}) + (1.5\text{ft} - h)A_j]$$

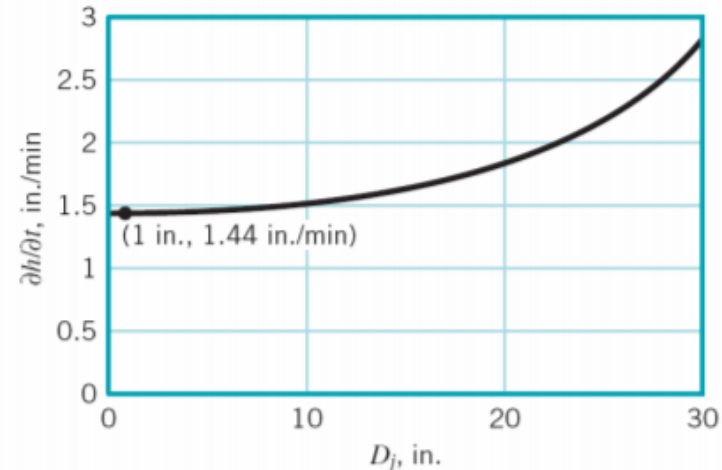
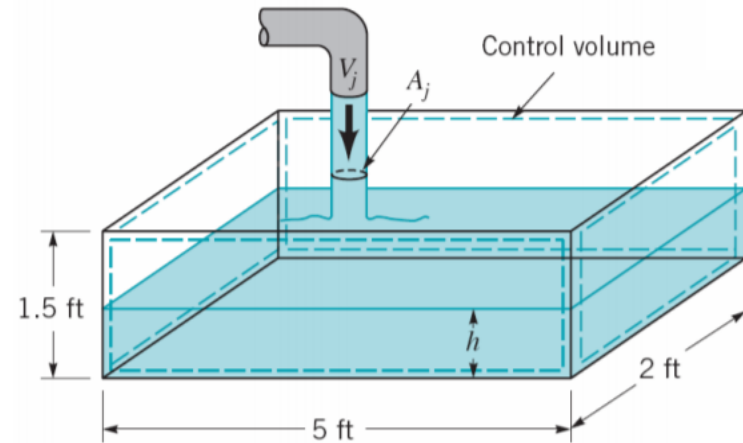
$$\Rightarrow \rho_{\text{water}} (10\text{ft}^2 - A_j) \frac{\partial h}{\partial t} = \dot{m}_{\text{water}}$$

and, thus

$$\frac{\partial h}{\partial t} = \frac{Q_{\text{water}}}{(10\text{ft}^2 - A_j)}$$

For $A_j \ll 10\text{ft}^2$ we can conclude that

$$\frac{\partial h}{\partial t} = \frac{Q_{\text{water}}}{(10\text{ft}^2)} = \frac{(9\text{ gal/min})(12\text{ in./ft})}{(7.48\text{ gal/ft}^3)(10\text{ft}^2)} = 1.44\text{ in./min}$$



□ Integral Form of the Mas Conservation Equation

A balloon is being inflated with an air supply by a small tube. The velocity within the 1-cm-diameter tube is 10 m/s.

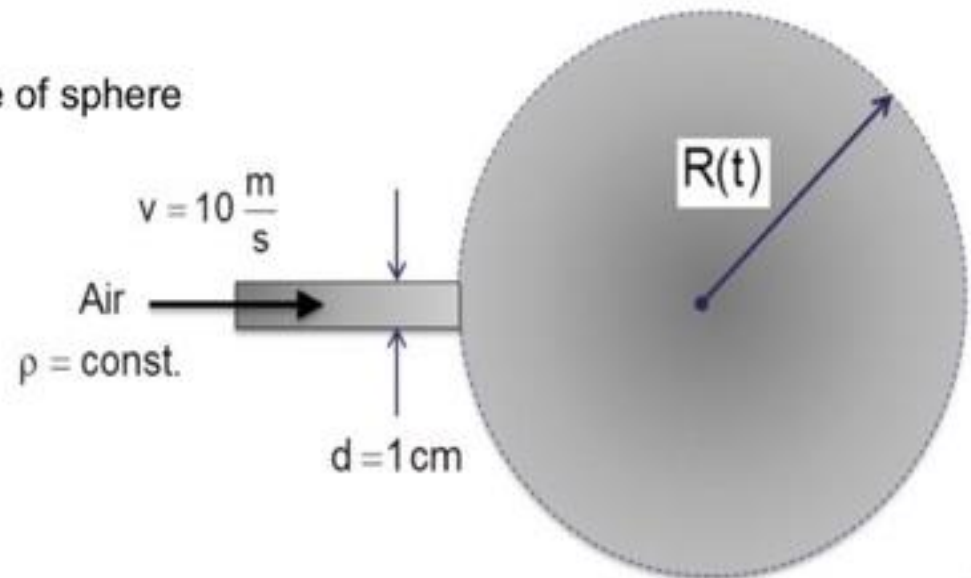
Find the rate of growth of the radius R at the instant when $R = 0.5$ m.

Given:

Surface of a sphere $A_{\text{Sphere}} = 4 \pi R^2$ *Ballon volume* $= \frac{4}{3} \pi R^3$

Assumption:

- Density of air remain constant
- Cross-sectional area of tube \ll Surface of sphere



Integral Form of the Mass Conservation Equation

Solution

It is convenient to define a deformable control surface just outside the balloon, expanding at the same rate $R(t)$. Equation (3.16) applies with $V_r = 0$ on the balloon surface and $V_r = V_1$ at the pipe entrance. For mass change, we take $B = m$ and $\beta = dm/dm = 1$. Equation (3.16) becomes

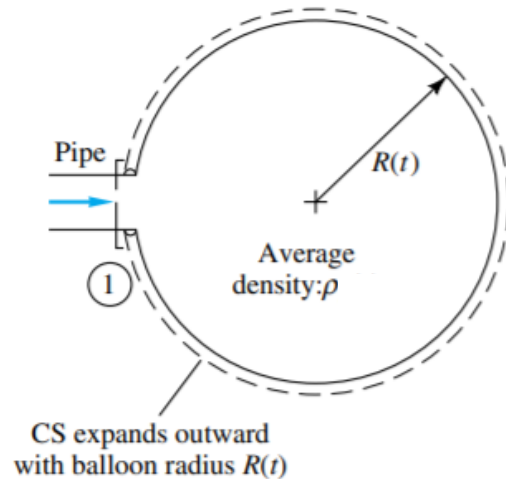
$$\left. \frac{Dm}{Dt} \right|_{system} = \frac{\partial}{\partial t} \int_{C.V.} \rho dV + \int_{C.S.} (\rho \vec{V}) \cdot d\vec{A} = 0$$

Mass flux occurs only at the inlet, so that the control-surface integral reduces to the single negative term $-\rho_1 A_1 V_1$. The fluid mass within the control volume is approximately the average density times the volume of a sphere. The equation thus becomes

$$\left. \frac{Dm}{Dt} \right|_{system} = \frac{\partial}{\partial t} \left(\frac{4}{3} \pi R^3 \rho \right) + \int_{C.S.} (\rho \vec{V}) \cdot d\vec{A} = 0$$

$$\Rightarrow \frac{4}{3} \pi \rho \frac{\partial R^3}{\partial t} - \rho V_1 A_1 = 0$$

$$\Rightarrow \frac{\partial R}{\partial t} = \frac{V_1 A_1}{4\pi R^2} = \frac{V_1 * \pi r_1^2}{4\pi R^2} = \frac{V_1 * r_1^2}{4R^2} = \frac{10 * 0.005^2}{4 * 0.5^2} = 2.5 \times 10^{-4} \text{ m/s}$$



Integral Form of the Mass Conservation Equation

$$\left. \frac{Dm}{Dt} \right|_{\text{system}} = \frac{\partial}{\partial t} \int_{C.V.} \rho dV + \int_{C.S.} (\rho \vec{V}) \cdot d\vec{A} = 0$$

- Chose the control volume inside the balloon
- Flow velocity will be the same as the balloon radius growth rate

$$\frac{dR}{dt} = V_2$$

- Flow inside the control volume is steady, therefore:

$$\left. \frac{Dm}{Dt} \right|_{\text{system}} = \frac{\partial}{\partial t} \int_{C.V.} \rho dV + \int_{C.S.} (\rho \vec{V}) \cdot d\vec{A} = 0$$

$$\left. \frac{Dm}{Dt} \right|_{\text{system}} = 0 + \int_{C.S.} (\rho \vec{V}) \cdot d\vec{A} = 0$$

$$\Rightarrow \rho A_2 V_2 - \rho V_1 A_1 = 0$$

$$\Rightarrow \rho 4\pi R^2 \frac{\partial R}{\partial t} - \rho V_1 \pi r_1^2 = 0$$

$$\Rightarrow \frac{\partial R}{\partial t} = V_2 = \frac{V_1 * \pi r_1^2}{4\pi R^2} = \frac{V_1 * r_1^2}{4R^2} = \frac{10 * 0.005^2}{4 * 0.5^2} = 2.5 \times 10^{-4} \text{ m/s}$$

