Lecture #07: Conservation of Momentum

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Reynolds Transport Theorem



Where α is any intensive property corresponding to N. (i.e., $\alpha = N$ per unit mass), and it can be used for different quantities as follows.

0

$N_{\scriptscriptstyle S}$	α
Mass	1
Linear momentum	\vec{V}
Angular momentum	$\vec{R} \times \vec{V}$
Energy	е
Entropy	S



Conservation of Momentum

Newton's second law states that:

[Time change rate of momentum of a system] = [Resultant external force acting on the system]

$$\frac{d\vec{M}_{S}}{dt} = \sum \vec{F}_{S} = \sum \vec{F}_{Surface} + \sum \vec{F}_{body}$$

Reynolds Transport Theorem:

Λ

$$\frac{dN_s}{dt}\Big|_{system} = \frac{d\int_{\Psi} \alpha \rho \, d\Psi}{Dt} = \frac{\partial}{\partial t} \int_{C.V.} \alpha \rho \, d\Psi + \int_{C.S.} (\alpha \rho \vec{V}) \bullet d\vec{A}$$

$$Make: \quad \alpha = \vec{V} \qquad \Rightarrow \frac{DM_s}{Dt}\Big|_{system} = \frac{\partial}{\partial t} \int_{C.V.} \rho \vec{V} \, d\Psi + \int_{C.S.} (\vec{V} \rho \vec{V}) \bullet d\vec{A} = 0$$

Integral form of the Mass Conservation Equation:

$$\frac{\partial}{\partial t} \int_{C.V.} \vec{V} \rho \, d\Psi + \int_{C.S.} (\vec{V} \rho \vec{V}) \bullet d\vec{A} = \sum \vec{F}_{surface} + \sum \vec{F}_{body}$$



System

$$\frac{\partial}{\partial t} \int_{C.V.} \vec{V} \rho \, d\Psi + \int_{C.S.} (\vec{V} \rho \vec{V}) \bullet d\vec{A} = \sum \vec{F}_{surface} + \sum \vec{F}_{body}$$

 $\vec{F}_{surface}$

 $\vec{F}_{\textit{body}}$

Surface forces such as pressure and shear stress. The surface forces usually expressed as $\vec{F}_{surface} = \int_{C.S.} \widetilde{P} \bullet d\vec{A}$, where \widetilde{P} is the stress tensor exerted by the surroundings on the particle surface. $\widetilde{P} = -P\widetilde{I} + \widetilde{\tau}$



Body forces such as electromagnetic, gravitational forces. <u>Usually</u> the body force can be expressed as $\vec{F}_{body} = \int_{CV} \rho \vec{f} \, dV$, where \vec{f} is a vector which references the resultant force per unit mass.

• Integral form of the Momentum Conservation Equation

$$\frac{\partial}{\partial t} \int_{C.V.} \rho \vec{V} \, d\Psi + \int_{C.S.} (\rho \vec{V} \vec{V}) \bullet d\vec{A} = \int_{C.S.} \tilde{P} \bullet d\vec{A} + \int_{C.V.} \rho \vec{f} \, d\Psi$$



Flow past a pipe bend



 Consider the pipe bend shown above. We may first draw a free body diagram for the control volume with the forces:



Problem Solution:

- 1. Chose a control volume:
- 2. Applying momentum conservation equation.

$$\frac{\partial}{\partial t} \int_{C.V.} \vec{V} \rho \, d\Psi + \int_{C.S.} (\vec{V} \rho \vec{V}) \bullet d\vec{A} = \sum \vec{F}_{surface} + \sum \vec{F}_{body}$$

Paying due regard to the positive x and y directions, we may write the summation of forces in these two directions:

$$\sum F_x = p_1 A_1 - p_2 A_2 \cos \theta - F_2$$
$$\sum F_y = F_y - p_2 A_2 \sin \theta - W$$

Relating these components to the net change of momentum flux through the inlet and exit surfaces

x-Direction

$$p_1A_1 - p_2A_2\cos\theta - F_x = \rho Q \left(\overline{V}_2\cos\theta - \overline{V}_1\right)$$

y-Direction

$$F_y - p_2 A_2 \sin \theta - W = \rho Q \left(\overline{V}_2 \sin \theta - 0 \right)$$

$$F = \sqrt{F_x^2 + F_y^2}$$
$$\phi = \tan^{-1} \left(F_y / F_x \right)$$



As a reaction, the impact force on the pipe bend is equal in magnitude, but opposite in direction to the one on the fluid.

Example Problem:

A static thrust stand as shown in the Figure is to be designed for testing a jet engine. The flow conditions are known for a typical test: The intake flow velocity = 200m/s; exhaust gas velocity = 500 m/s; inlet cross-section area = 1.0 m²; intake static pressure = -22.5 kPa (gauge) = 78.5 kPa(absolute); intake temperature = 268K; exhaust static pressure = 0 kPa =101 kPa(absolute). **Estimate the thrust force generated by the jet engine on a static thrust stand.**



Problem Solution:

- 1. Chose a control volume:
- 2. Applying momentum conservation equation

$$\frac{\partial}{\partial t} \int_{C.V.} \vec{V} \rho \, d\Psi + \int_{C.S.} (\vec{V} \rho \vec{V}) \bullet d\vec{A} = \sum \vec{F}_{surface} + \sum \vec{F}_{body}$$



•Since the flow is steady, the momentum equation is simplified as:

$$\int_{C.S.} (\vec{V} \,\rho \,\vec{V}) \bullet d\vec{A} = \sum \vec{F}_{surface} + \sum \vec{F}_{body}$$

• Forces along X- direction:

$$\sum F_x = F_{thrust} + P_1 A_1 - P_2 A_2$$

• Momentum along X- direction:



$$\int_{C.S.} (u \rho \vec{V}) \bullet d\vec{A} = \int_{A_1} (u_1 \rho \vec{V}) \bullet d\vec{A} + \int_{A_2} (u \rho \vec{V}) \bullet d\vec{A} = -V_1 \rho_1 A_1 V_1 + V_2 \rho_2 A_2 V_2$$

based on consevation of mass \Rightarrow mass flowrate $\dot{m} = \rho_1 A_1 V_1 = \rho_2 A_2 V_2$ Therefore: $\int_{C.S.} (u \rho \vec{V}) \bullet d\vec{A} = \dot{m} (V_2 - V_1) \Rightarrow F_{thrust} = \dot{m} (V_2 - V_1) - P_1 A_1 + P_2 A_2$

Problem Solution - continue:

- 1. Chose a control volume:
- 2. Applying momentum conservation equation

$$F_{thrust} = \dot{m} (V_2 - V_1) - P_1 A_1 + P_2 A_2$$

$$V_{1} = 200m / s$$

$$P_{1} = -22.5kPa(gauge) = 78.5kPa(absolute)$$

$$\rho_{1} = \frac{P_{1}}{RT_{1}} = \frac{78.5 \times 10^{3}}{287.5 \times 268} = 1.02 \ kg / m^{3}$$

$$\dot{m} = \rho_{1}V_{1}A_{1} = 1.02 \times 200 \times 1.0 = 204 \ kg / s$$

$$V_{2} = 500m / s$$
Therefore:
$$F_{thrust} = \dot{m}(V_{2} - V_{1}) - P_{1}A_{1} + P_{2}A_{2}$$

$$= 204 \times (500 - 200) - (-22.5 \times 10^{3} \times 1.0) + 0 \times 10^{3}$$

= 61200 + 22500

= 83700N





Example-Drag on an airfoil

Airfoil aerodynamics

https://www.youtube.com/watch?v=8fk2J5LtdSg





 Problem : Two-dimensional steady flow around the airfoil where velocity profile is given (measured) at upstream and a downstream location. Find an expression for the drag force on the airfoil.