

Lecture # 14: BERNOULLI EQUATION

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IDEAL FLOW

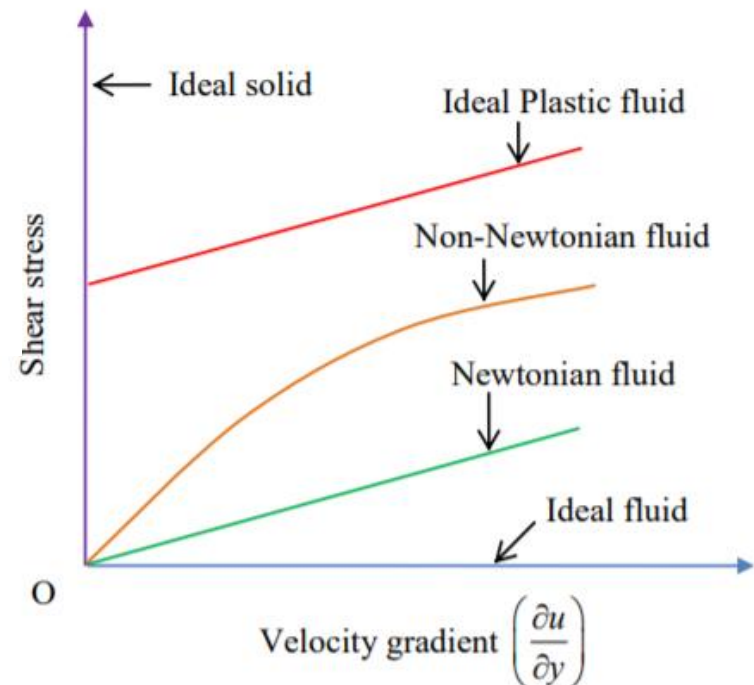
Ideal flow:

- **Non-heat conducting, inviscid, incompressible, homogeneous fluid is defined as ideal fluid.**
- **Assumptions used are:**
 - **Non-heat conductive**
 - **Homogeneous**
 - **Incompressible**
 - **Inviscid flow**

Controlling equations:

Continuity equation:

$$\frac{\partial \rho}{\partial t} + \nabla \cdot (\rho \vec{V}) = 0 \Rightarrow \frac{\partial \rho}{\partial t} + \vec{V} \cdot \nabla \rho + \rho \nabla \cdot \vec{V} = 0$$
$$\Rightarrow \frac{D\rho}{Dt} + \rho \nabla \cdot \vec{V} = 0$$
$$\Rightarrow \nabla \cdot \vec{V} = 0$$



□ GOVERNING EQUATIONS FOR IDEAL FLUID FLOWS

Momentum equation:
$$\frac{\partial(\rho \vec{V})}{\partial t} + \nabla \cdot (\rho \vec{V} \vec{V}) + \nabla P - \nabla \cdot \vec{\tau} - \rho \vec{f} = 0$$

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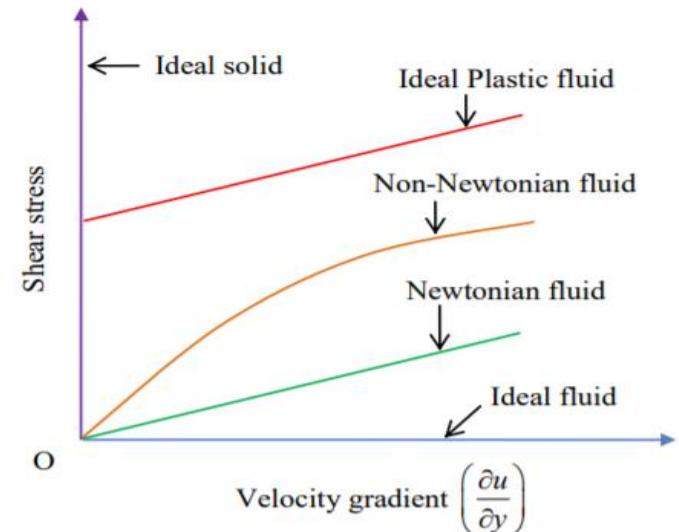
$$\Rightarrow \vec{V} \frac{\partial \rho}{\partial t} + \rho \frac{\partial \vec{V}}{\partial t} + \vec{V} \nabla \cdot (\rho \vec{V}) + (\rho \vec{V} \cdot \nabla) \vec{V} + \nabla P - \overbrace{\nabla \cdot \vec{\tau}}^{=0 \text{ due to inviscid}} - \rho \vec{f} = 0$$

$$\Rightarrow \vec{V} \left[\frac{\partial \rho}{\partial t} + \nabla \cdot (\rho \vec{V}) \right] + \rho \left[\frac{\partial \vec{V}}{\partial t} + (\vec{V} \cdot \nabla) \vec{V} \right] + \nabla P - \overbrace{\nabla \cdot \vec{\tau}}^{=0 \text{ due to inviscid}} - \rho \vec{f} = 0$$

$$\Rightarrow \rho \frac{D\vec{V}}{Dt} = -\nabla P + \rho \vec{f}$$

$$\rho \frac{D\vec{V}}{Dt} = -\nabla P + \rho \vec{f}$$

is also called Euler equation

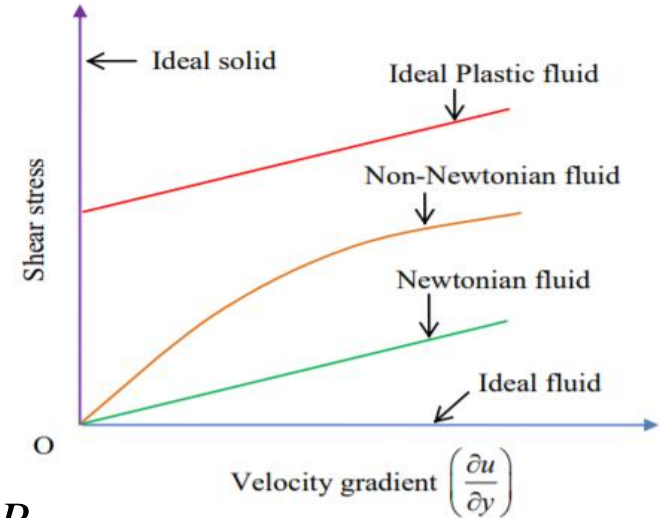


□ GOVERNING EQUATIONS FOR IDEAL FLUID FLOWS

For ideal fluid, the governing equations are:

1). Continuity equation: $\nabla \cdot \vec{V} = 0$

2). Euler equation $\rho \frac{D\vec{V}}{Dt} = -\nabla P + \rho \vec{f}$
 or $\frac{D\vec{V}}{Dt} = -\nabla\left(\frac{P}{\rho}\right) + \vec{f}$



- **For the Euler equation, it can also be re-written as:**

$$\frac{D\vec{V}}{Dt} = -\nabla\left(\frac{P}{\rho}\right) + \vec{f} \quad \Rightarrow \quad \frac{\partial \vec{V}}{\partial t} + (\vec{V} \cdot \nabla)\vec{V} = -\nabla\left(\frac{P}{\rho}\right) + \vec{f}$$

Since $(\vec{V} \cdot \nabla)\vec{V} = \nabla\left(\frac{\vec{V} \cdot \vec{V}}{2}\right) - \vec{V} \times (\nabla \times \vec{V}) \Rightarrow \frac{\partial \vec{V}}{\partial t} + \nabla\left(\frac{\vec{V} \cdot \vec{V}}{2} + \frac{P}{\rho}\right) - \vec{V} \times (\nabla \times \vec{V}) = \vec{f}$

- **Let us only consider body forces that are conservative only. A necessary and sufficient condition for the body force can be represented as the gradient of a scalar field U, i.e.,**

$$\vec{f} = \nabla U$$

- **Therefore:**

$$\frac{\partial \vec{V}}{\partial t} + \nabla\left(\frac{\vec{V} \cdot \vec{V}}{2} + \frac{P}{\rho}\right) - \vec{V} \times (\nabla \times \vec{V}) = \nabla U \quad \Rightarrow \quad \frac{\partial \vec{V}}{\partial t} + \nabla\left(\frac{\vec{V} \cdot \vec{V}}{2} + \frac{P}{\rho} - U\right) - \vec{V} \times (\nabla \times \vec{V}) = 0$$

□ Integral of Euler Equation in Irrotational Flows

$$\frac{\partial \vec{V}}{\partial t} + \nabla \left(\frac{\vec{V} \cdot \vec{V}}{2} + \frac{P}{\rho} \right) - \vec{V} \times (\nabla \times \vec{V}) = \nabla U \quad \Rightarrow \quad \frac{\partial \vec{V}}{\partial t} + \nabla \left(\frac{\vec{V} \cdot \vec{V}}{2} + \frac{P}{\rho} - U \right) - \vec{V} \times (\nabla \times \vec{V}) = 0$$

- If the flow is **irrotational, then** $\nabla \times \vec{V} = 0$ $\vec{f} = \nabla U$
- The above equation can be simplified as: $\frac{\partial \vec{V}}{\partial t} + \nabla \left(\frac{\vec{V} \cdot \vec{V}}{2} + \frac{P}{\rho} - U \right) = 0$
- If the flow is steady: $\Rightarrow \nabla \left(\frac{\vec{V} \cdot \vec{V}}{2} + \frac{P}{\rho} - U \right) = 0$ $\vec{f} = \nabla U$
- By the definition of directional derivative **along any arbitrary path**: $\nabla() \cdot d\vec{l} = d()$
- Therefore: $\nabla \left(\frac{\vec{V} \cdot \vec{V}}{2} + \frac{P}{\rho} - U \right) \cdot d\vec{l} = d \left(\frac{\vec{V} \cdot \vec{V}}{2} + \frac{P}{\rho} - U \right) = 0$
- Integrating the above equation leads to the unsteady **Bernoulli equation:**

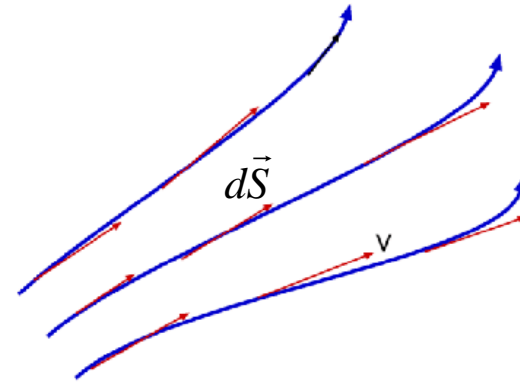
$$\int d \left(\frac{\vec{V} \cdot \vec{V}}{2} + \frac{P}{\rho} - U \right) = 0 \quad \Rightarrow \quad \frac{\vec{V} \cdot \vec{V}}{2} + \frac{P}{\rho} - U = \text{const.}$$

□ Integral of Euler Equation along a Streamline

$$\frac{\partial \vec{V}}{\partial t} + \nabla \left(\frac{\vec{V} \cdot \vec{V}}{2} + \frac{P}{\rho} \right) - \vec{V} \times (\nabla \times \vec{V}) = \nabla U \quad \Rightarrow \quad \frac{\partial \vec{V}}{\partial t} + \nabla \left(\frac{\vec{V} \cdot \vec{V}}{2} + \frac{P}{\rho} - U \right) - \vec{V} \times (\nabla \times \vec{V}) = 0$$

- **For the steady flow:** $\frac{\partial \vec{V}}{\partial t} = 0$

- **Then:** $\nabla \left(\frac{\vec{V} \cdot \vec{V}}{2} + \frac{P}{\rho} - U \right) = \vec{V} \times (\nabla \times \vec{V})$



- **Multiple (dot product) both sides of the above equation by, $d\vec{S}$ which is an element length **along a streamline**.**

- **Therefore:** $\nabla \left(\frac{\vec{V} \cdot \vec{V}}{2} + \frac{P}{\rho} - U \right) \cdot d\vec{S} = \vec{V} \times (\nabla \times \vec{V}) \cdot d\vec{S}$

- **Since:** $\vec{V} \times (\nabla \times \vec{V}) \cdot d\vec{S} = d\vec{S} \cdot [\vec{V} \times (\nabla \times \vec{V})] = (\nabla \times \vec{V}) \cdot (d\vec{S} \times \vec{V}) = 0$

- **Therefore:** $\nabla \left(\frac{\vec{V} \cdot \vec{V}}{2} + \frac{P}{\rho} - U \right) \cdot d\vec{S} = 0 \quad \Rightarrow \quad d \left(\frac{\vec{V} \cdot \vec{V}}{2} + \frac{P}{\rho} - U \right) = 0$

- **Bernoulli equation **along a streamline**:** $\frac{\vec{V} \cdot \vec{V}}{2} + \frac{P}{\rho} - U = \text{const } C$

□ Integral of Euler Equation in Irrotational Flows

- If we choose a Cartesian coordinate system with the Z-axis to be positive when pointing upward and normal to the surface of the earth,. The force on a body of mass “m” is given by $(0,0,-mg)$. Thus, the body force vector per unit mass becomes: $\vec{f} = (f_x, f_y, f_z) = (0, 0, -g)$

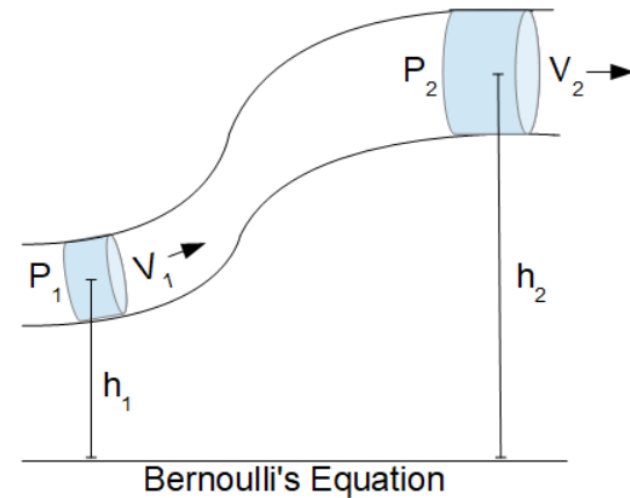
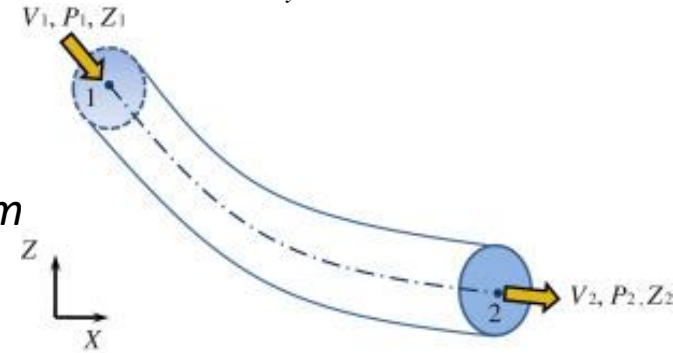
$$\frac{\partial U}{\partial Z} = -g \quad \Rightarrow \quad U = -g Z$$

- Therefore, **Bernoulli equation** for irrotational flow becom

$$\frac{\vec{V} \cdot \vec{V}}{2} + \frac{P}{\rho} - U = Const.$$

$$\Rightarrow \frac{\vec{V} \cdot \vec{V}}{2} + \frac{P}{\rho} + gz = Const.$$

- Stagnation point:**
 - the point on a streamline with the flow velocity becoming zero.
- Total pressure:**
 - The pressure measured at the stagnation point.

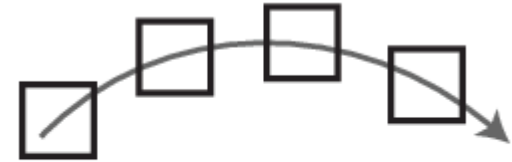


□ BERNOLLI EQUATION

- **Bernoulli equation:**

$$\frac{\vec{V} \cdot \vec{V}}{2} + \frac{P}{\rho} + gz = \text{Const.}$$

- *We can derive Bernoulli's equation for an irrotational flow without having to limit the equation to a streamline.*
- *If flow is irrotational and steady (above case), Bernoulli's equation applies, and the constant is the same everywhere in the flow.*
- *If flow is rotational but steady, Bernoulli's equation holds along a streamline. The value of constant is different for each streamline.*
- *If flow is irrotational and unsteady, a modified version of Bernoulli's equation applies, and the constant is the same throughout the flow (We don't cover this in AERE 310).*
- *If flow is rotational and unsteady, Bernoulli's equation is no longer valid (Full Euler's equation must be solved).*

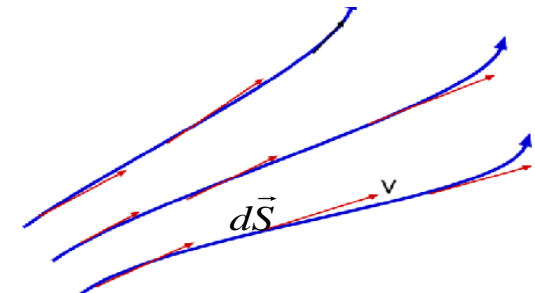


irrotational

- **Applicable everywhere in irrotational flows**



rotational



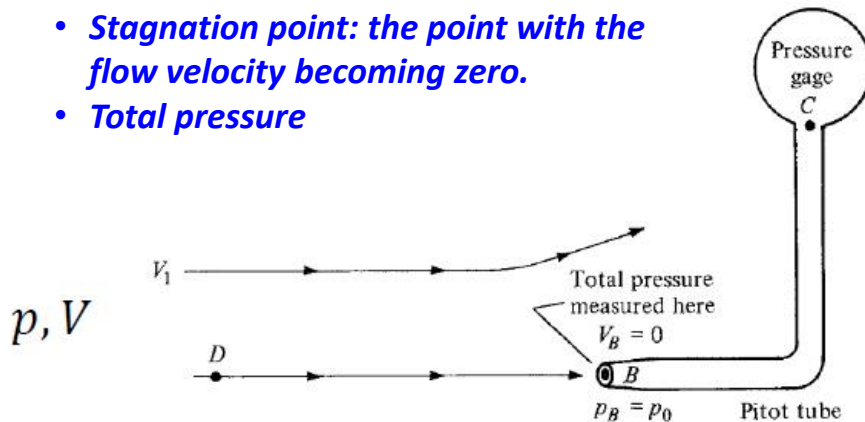
- **Along the streamline in rotational flows**

□ BERNOULLI EQUATION FOR IRROTATIONAL FLOW

- The most common instrument for measuring airspeed in airplanes.

Consider a flow with pressure p and velocity V approaching a pitot tube:

- *Stagnation point: the point with the flow velocity becoming zero.*
- *Total pressure*



Bernoulli's equation between point D and B

□ BERNULLI EQUATION FOR IRROTATIONAL FLOW

Pitot tube

- Bernoulli's equation between point D and B

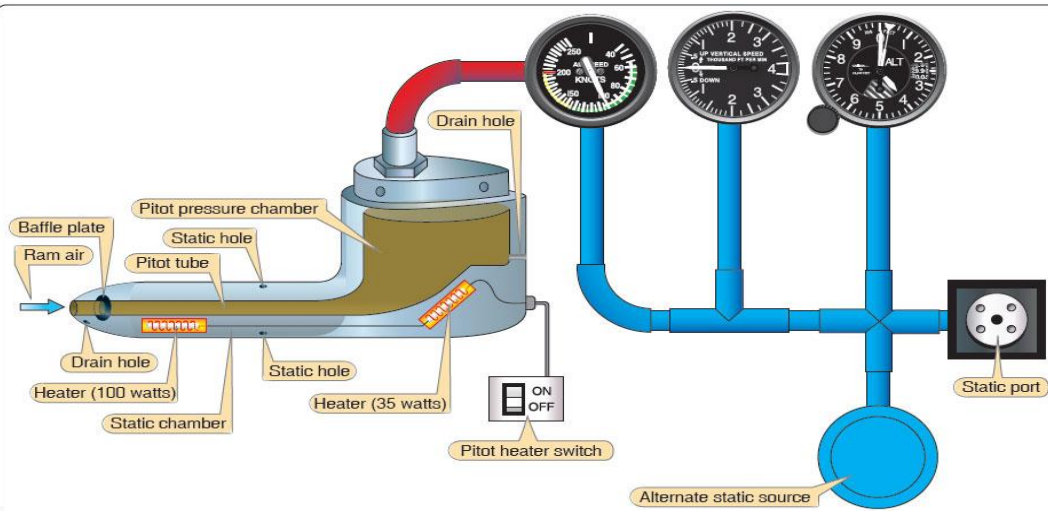
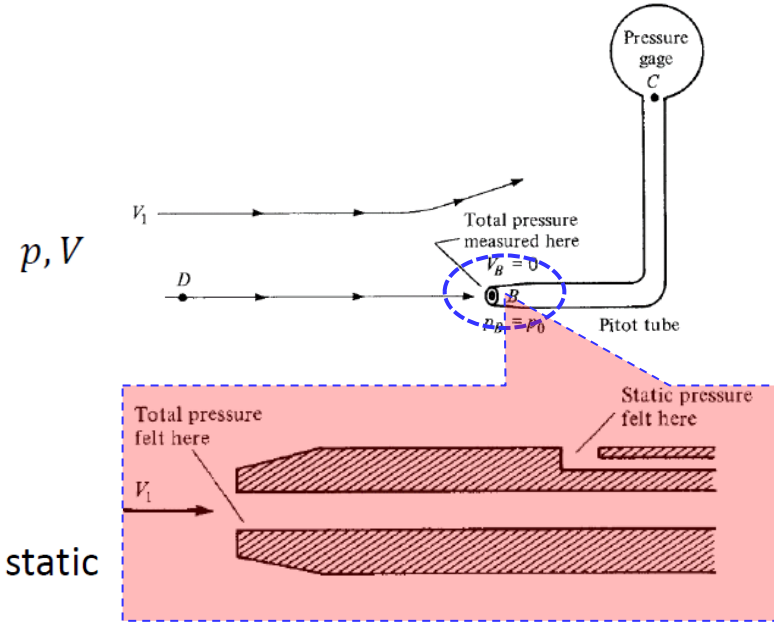
$$p + \rho \frac{V^2}{2} = p_B + \rho \frac{V_B^2}{2}$$

But $V_B = 0$ and by definition $p_B = p_0$ or stagnation pressure

Therefore:

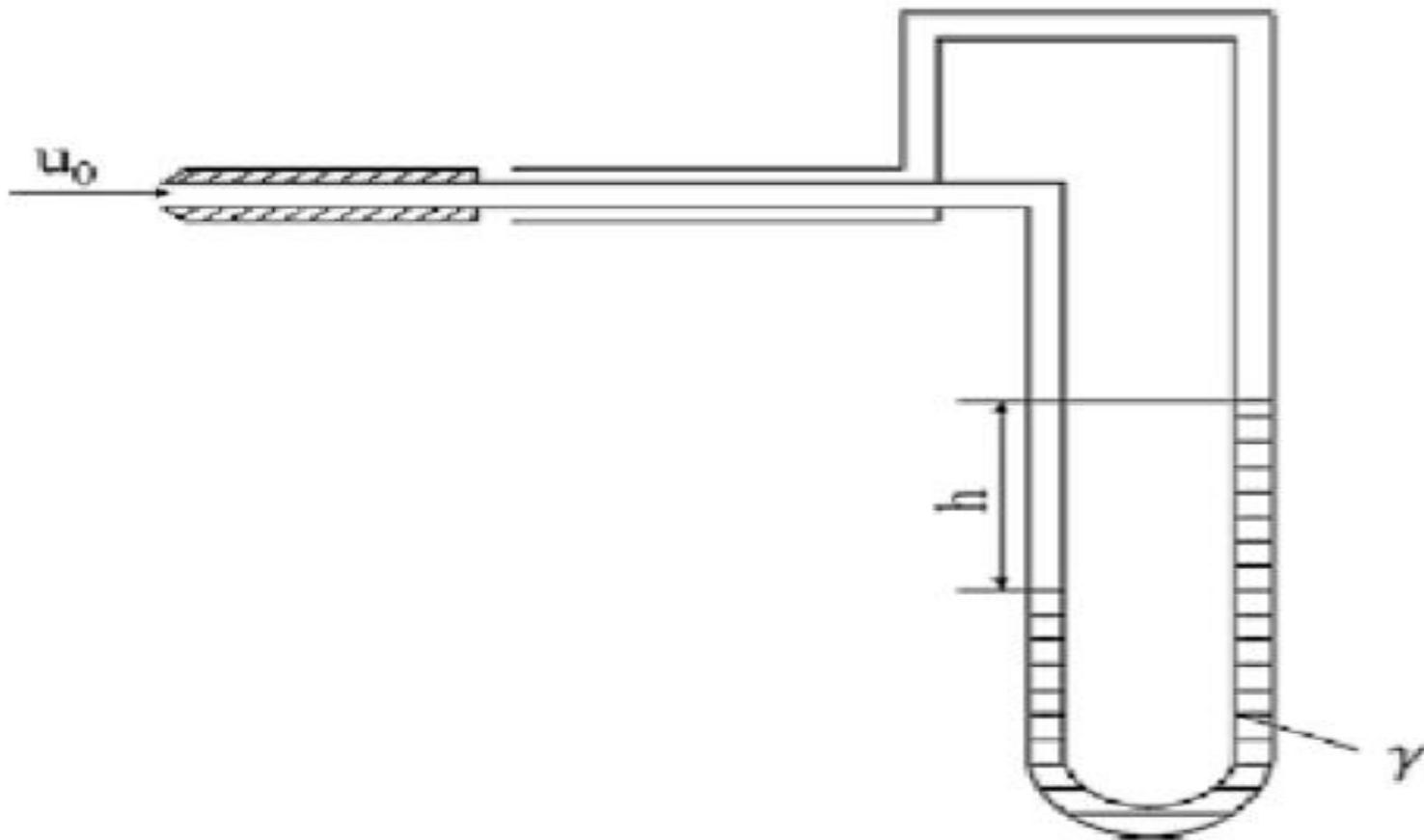
$$V = \sqrt{\frac{2(p_0 - p)}{\rho}}$$

- By measuring the difference between total (stagnation) and static pressure, we can calculate the flow velocity.
- Often a Pitot-static probe is used to measure both pressures



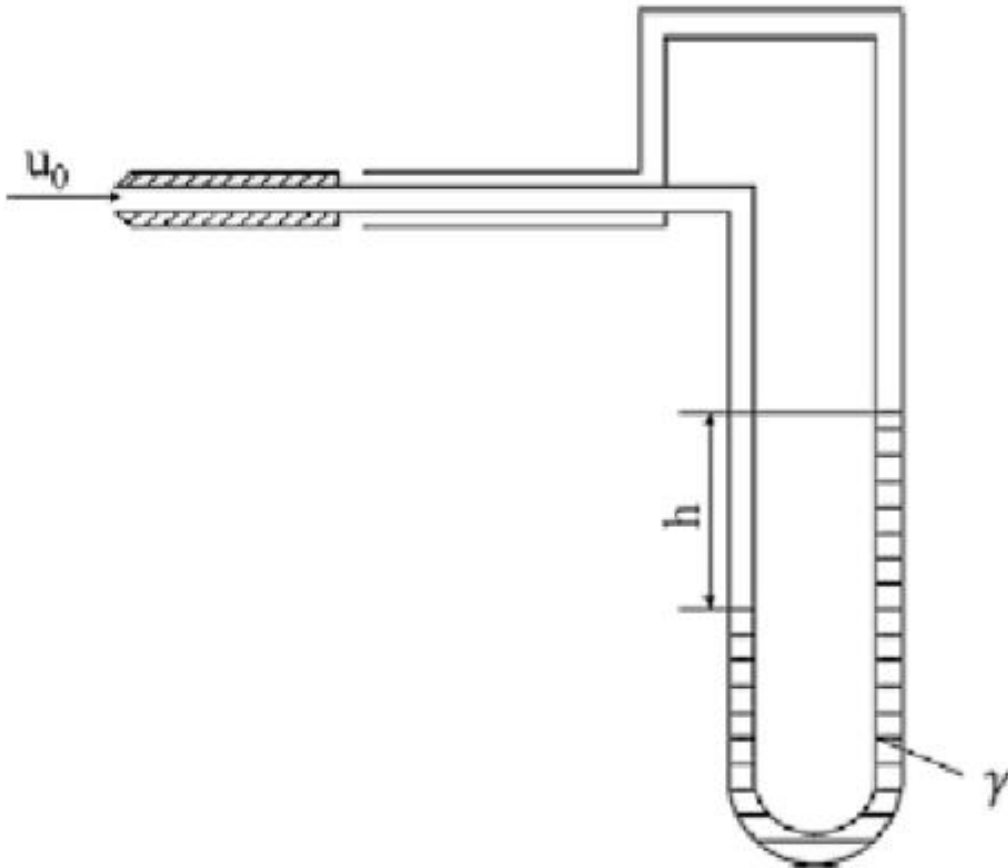
□ BERNULLI EQUATION FOR IRROTATIONAL FLOW

A Pitot tube connected to a water manometer is used to measure the air velocity in the pipe, as shown in Fig. 3.35. The reading of the manometer is $h = 150 \text{ mm H}_2\text{O}$. The air density is $\rho_a = 1.20 \text{ kg/m}^3$, and the water density is $\rho = 1000 \text{ kg/m}^3$. The velocity coefficient of Pitot tube is $c = 1$. Neglecting the energy loss, try to determine the air velocity u_0 .



□ BERNOULLI EQUATION FOR IRROTATIONAL FLOW

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Based on Bernoulli equation:

$$\frac{\vec{V} \cdot \vec{V}}{2} + \frac{P}{\rho} = \text{Constant}$$

$$\Rightarrow \frac{V_0^2}{2} + \frac{P_0}{\rho_{air}} = \frac{V_1^2}{2} + \frac{P_1}{\rho_{air}}$$

$$\Rightarrow \frac{V_0^2}{2} + \frac{P_0}{\rho_{air}} = \frac{P_1}{\rho_{air}}$$

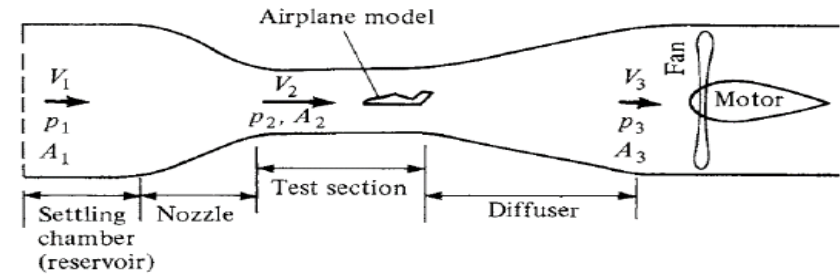
$$\Rightarrow V_0 = \sqrt{\frac{2(P_1 - P_0)}{\rho_{air}}} = \sqrt{\frac{2H \rho_{water} g}{\rho_{air}}}$$

$$= \sqrt{\frac{2 * 0.15 * 1000 * 9.8}{1.20}} \approx 49.5 \text{ m/s}$$

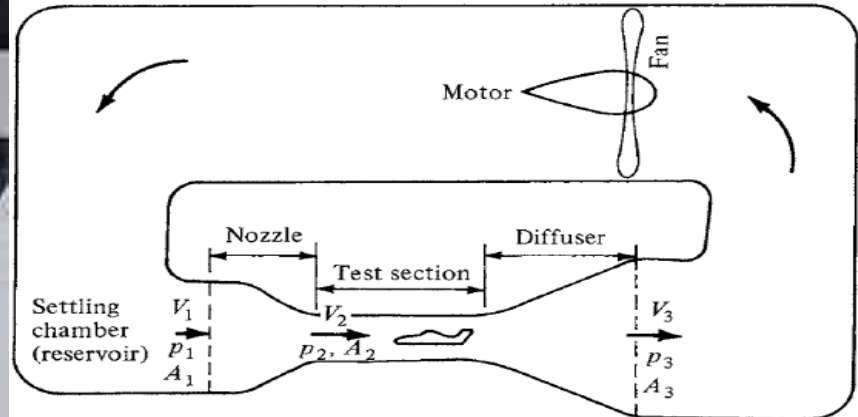
□ BERNULLI EQUATION FOR IRROTATIONAL FLOW

The flow velocity in the test section of a low-speed wind tunnel is 100 mph. The test section is vented to the atmosphere, where atmospheric pressure is $1.01 \times 10^5 \text{ N/m}^2$. The air density is 1.23 kg/m^3 . The contraction ratio of the nozzle is 10 to 1.

- (a) Calculate the reservoir pressure in atmosphere.
- (b) By how much must the reservoir pressure be increased to achieve 200 mph in the test section?



(a) Open-circuit tunnel



(b) Closed-circuit tunnel

□ BERNULLI EQUATION FOR IRROTATIONAL FLOW

Conservation of mass

$$\rho V_1 A_1 = \rho V_2 A_2 = \rho V_3 A_3$$

Therefore

$$V_2 = \frac{A_1}{A_2} V_1 \text{ and } V_3 = \frac{A_2}{A_3} V_2$$

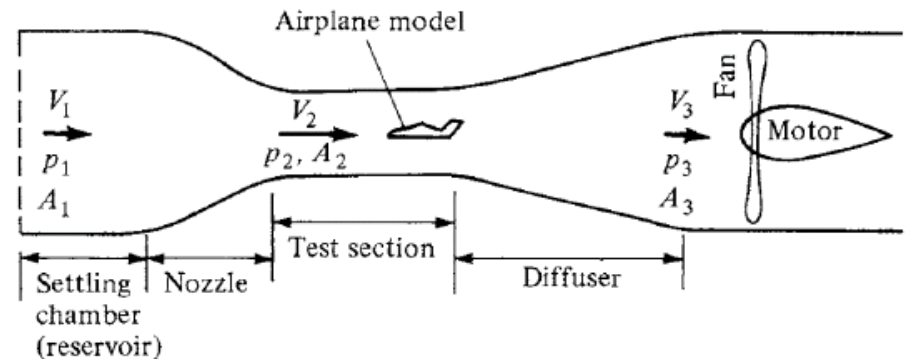
Bernoulli's equation

$$p_1 + \frac{1}{2} \rho V_1^2 = p_2 + \frac{1}{2} \rho V_2^2$$

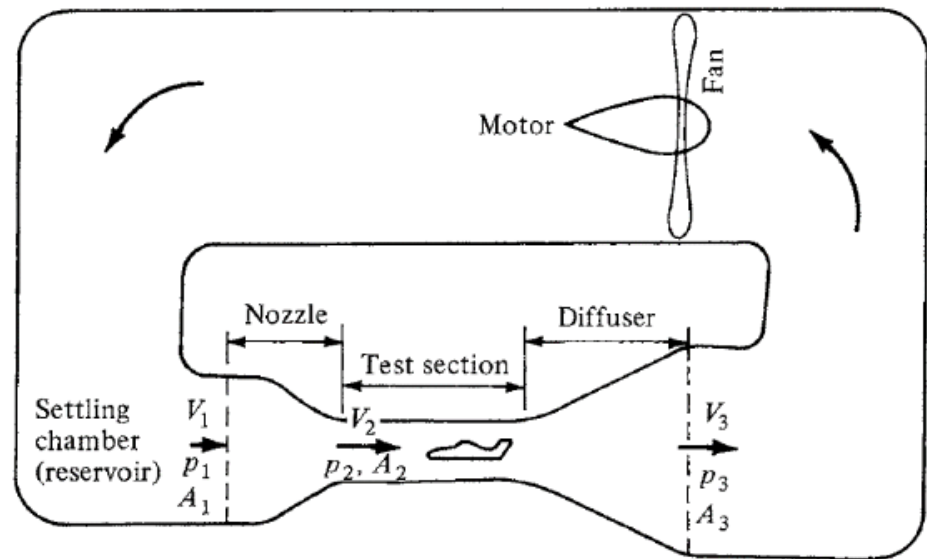
$$= p_3 + \frac{1}{2} \rho V_3^2$$

$$V_2^2 = \frac{2}{\rho} (p_1 - p_2) + V_1^2$$

$$V_2 = \sqrt{\frac{2(p_1 - p_2)}{\rho \left[1 - \left(\frac{A_2}{A_1} \right)^2 \right]}}$$



(a) Open-circuit tunnel



(b) Closed-circuit tunnel



BERNOULLI EQUATION FOR IRROTATIONAL FLOW

(a).

We have $V_2 = 100 \text{ mph}$, $\frac{A_1}{A_2} = 10$, $p_2 = 1.01 \times 10^5 \text{ Pa}$

Need to find p_1

$$p_1 - p_2 = \frac{1}{2} \rho V_2^2 \left[1 - \left(\frac{A_2}{A_1} \right)^2 \right]$$

Note $V_2 = 100 \text{ mph} = 100 \times \frac{0.447 \text{ m/s}}{1 \text{ mph}} = 44.7 \text{ m/s}$

$$p_1 - p_2 = \frac{1.23}{2} (44.7)^2 \left[1 - \left(\frac{1}{10} \right)^2 \right] = 0.01217 \times 10^5 \text{ Pa}$$

$$p_1 = 1.01 \times 10^5 + 0.01217 \times 10^5 \text{ Pa}$$

$$p_1 = 1.022 \times 10^5 \text{ Pa} = 1.01 \text{ atm}$$

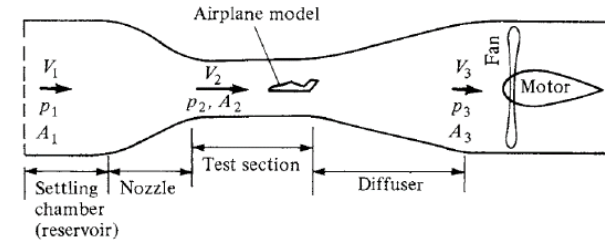
(b).

$V_2 = 200 \text{ mph} = 89.4 \text{ m/s}$

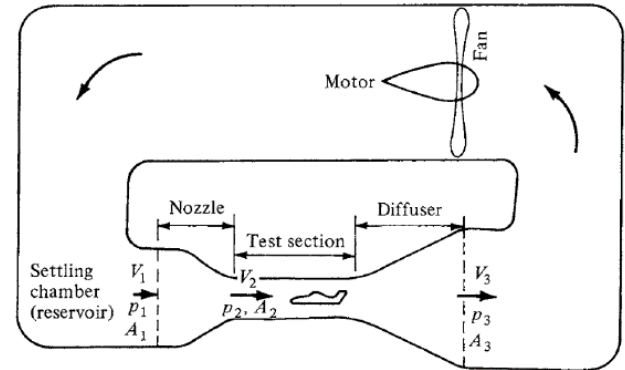
$$p_1 - p_2 = \frac{1.23}{2} (89.4)^2 \left[1 - \left(\frac{1}{10} \right)^2 \right] = 0.0487 \times 10^5 \text{ Pa}$$

$$p_1 = 1.01 \times 10^5 + 0.0487 \times 10^5 = 1.059 \times 10^5 \text{ Pa}$$

$$p_1 = 1.048 \text{ atm}$$



(a) Open-circuit tunnel



(b) Closed-circuit tunnel

Only a ~4% increase in pressure needed to increase velocity by 100%!

□ BERNOULLI EQUATION FOR IRROTATIONAL FLOW

- Understanding Bernoulli's Equation

<https://www.youtube.com/watch?v=DW4rItB20h4>

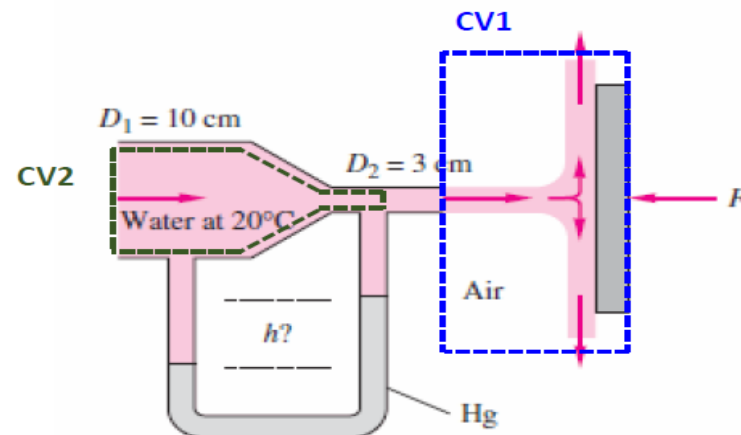


BERNOULLI'S
EQUATION

□ BERNOLLI EQUATION FOR IRROTATIONAL FLOW

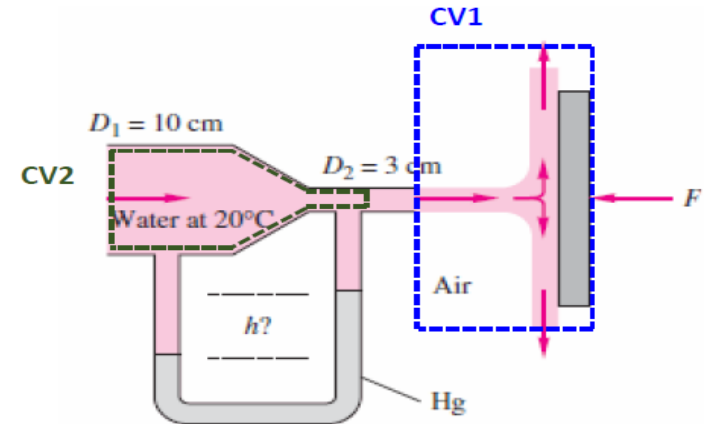
Examples involving Bernoulli's equation

- Water flows through a circular nozzle, exits into the air as a jet, and strikes a plate, as shown in Figure. The force required to hold the plate steady is $F=70$ N. Assuming steady, frictionless, one-dimensional flow, estimate
 - (a) The velocities at sections (1) and (2) and
 - (b) the mercury manometer reading h ($\rho_{Hg} = 13550$ kg/m³).



□ BERNULLI EQUATION FOR IRROTATIONAL FLOW

Example-solution



$p = p_{atm}$
everywhere

$f_x = 0$

- X-momentum for CV1

$$\frac{\partial}{\partial t} \iiint_V \rho u dV + \iint_S \rho u (\vec{V} \cdot \hat{n}) dS = \iiint_V \rho f_x dV + \iint_S p_x dS + \sum F_x$$

$= -F$

$= 0$ (steady)

$$-\rho_w u_2^2 A_2 = -F \rightarrow F = \frac{\pi}{4} \rho_w D_2^2 u_2^2$$

$$u_2 = \sqrt{\frac{4F}{\pi \rho_w D_2^2}} = \sqrt{\frac{4 \times 70}{\pi \times 1000 \times 0.03^2}} = 9.95 \text{ m/s}$$

- Conservation of mass for CV2

$$\rho_w u_1 A_1 = \rho_w u_2 A_2 \rightarrow u_1 = u_2 \frac{A_2}{A_1} = u_2 \left(\frac{D_2}{D_1} \right)^2$$

$$u_1 = 9.95 \left(\frac{3}{10} \right)^2 \rightarrow u_1 = 0.9 \text{ m/s}$$

□ BERNULLI EQUATION FOR IRROTATIONAL FLOW

Example-solution

- Bernoulli's equation on a streamline from 1 to 2

$$p_1 + \frac{1}{2} \rho_w u_1^2 = p_2 + \frac{1}{2} \rho_w u_2^2$$
$$\rightarrow p_1 - p_2 = \frac{1}{2} \rho_w (u_2^2 - u_1^2)$$

For the manometer

$$p_1 - \rho_{Hg} g h = p_2 \rightarrow p_2 - p_1 = \rho_{Hg} g h$$

Therefore

$$h = \frac{1}{2g} \frac{\rho_w}{\rho_{Hg}} (u_2^2 - u_1^2) = \frac{1}{2 \times 9.81} \frac{1000}{13550} (9.95^2 - 0.9^2)$$

$$h = 0.37 \text{ m}$$

